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- [Home](#)
- [Journals](#)
- [About Us](#)



[About this Journal](#) [Submit a Manuscript](#) [Table of Contents](#)

Journal Menu

- [About this Journal](#) ·
- [Abstracting and Indexing](#) ·
- [Advance Access](#) ·
- [Aims and Scope](#) ·
- [Annual Issues](#) ·
- [Article Processing Charges](#) ·
- [Articles in Press](#) ·
- [Author Guidelines](#) ·
- [Bibliographic Information](#) ·
- [Citations to this Journal](#) ·
- [Contact Information](#) ·
- [Editorial Board](#) ·
- [Editorial Workflow](#) ·
- [Free eTOC Alerts](#) ·
- [Publication Ethics](#) ·
- [Reviewers Acknowledgment](#) ·
- [Submit a Manuscript](#) ·
- [Subscription Information](#) ·
- [Table of Contents](#)

- [Open Special Issues](#) ·
- [Published Special Issues](#) ·
- [Special Issue Guidelines](#)

- [Abstract](#)
- [Full-Text PDF](#)
- [Full-Text HTML](#)
- [Full-Text ePUB](#)
- [Full-Text XML](#)
- [Linked References](#)
- [How to Cite this Article](#)

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Research Article

A Double Inverted F-Shape Patch Antenna for Dual-Band Operation

Abstract

A double inverted F-shape patch antenna is presented for dual-band operation. The proposed antenna is comprised of circular and rectangular slots on a printed circuit board of 40 mm × 40 mm × 1.6 mm with a 50 Ω microstrip transmission line. Commercially available high frequency structural simulator (HFSS) based on the finite element method (FEM) has been adopted in this investigation. It has a measured impedance bandwidths (2 : 1 VSWR) of 18.53% on the lower band and 7.8% on the upper band, respectively. It has achieved stable radiation efficiencies of 79.76% and 80.36% with average gains of 7.82 dBi and 5.66 dBi in the operating frequency bands. Moreover, numerical simulations have been indicated as an important uniformity with measured results.

1. Introduction

The raising demands of wireless communication systems enforce the improvement of dual-band antennas that have abilities to operate under different standards in different frequency bands. Advances in wireless communications have introduced tremendous demands in the antenna technology. It also paved the way for wide usage of mobile phones in modern society resulting in mounting concerns surrounding its harmful radiation [1, 2]. Microstrip patch antenna plays an important role as a harbinger in wireless communication systems and is gradually carrying out to face the changing demands of update antenna technology. Microstrip patch antennas are presently under concern for using in broadband communication systems due to their attractive characteristics, such as low profile, low cost, lightweight, wide frequency bandwidth, ease of fabrication, and easy integration with monolithic microwave integrated circuits [3, 4]. However, the limitations of the microstrip patch antennas are having narrow bandwidth, and for that reason the demand of the bandwidth enhancement is gradually rising in the practical applications [5]. In order to enhance its bandwidth, many approaches have been applied conventionally, such as using thick substrates with low dielectrics constant, impedance matching network, parasitic patches stacked on the top of the main patch [6], slots loaded on the patch, high dielectric constant substrate, and adopting short-circuit pin [7].

In [8], a rectangular slot antenna has been stated for dual frequency operation. Reference [9] has narrated a printed dipole antenna to cover dual band with U-slot arms. Reference [10] has been reported a low cost microstrip dipole antenna for wireless communications. In [11], a PIFA antenna has been presented for dual band operation with U-slot. Reference [12] has been mentioned a dual loop antenna for 2.4/5 GHz wireless LAN. A monopole antenna with double-T has been stated in [13] for 2.4/5.2 GHz WLAN operations. A dual polarized antenna has been mentioned in [14] for Ku-band application. Microstrip antennas on FR4 substrate material were discussed for UWB applications in [15, 16].

In this research, a double inverted F-shape 40 × 40 mm² patch antenna for dual-band operation has been proposed and investigated to increase the bandwidth and reduce the size at the same time. The effect on antenna resonances and other antenna parameters is concentrated due to slots on the patch and ground plane to design the proposed dual-band double inverted F-shape antenna with enhanced bandwidth and efficiency. Some techniques are employed such as increasing substrate thickness, changing patch by cutting rectangular slots, and cutting ground plane to achieve the resultant parameters such as impedance matching, gain, radiation pattern, and return loss. The results have been given a hint that the proposed antenna is appropriate for X-band and Ku-band applications.

2. Antenna Geometry and Optimization

The length and width of the patch antenna can be calculated from (1) narrated in [17]. While L and W are the length and width of the patch, c is the velocity of light, ϵ_r is

$$W = \frac{c}{2f_0} \sqrt{\frac{\epsilon_r + 1}{2}}, \quad (1)$$
$$L = \frac{c}{2f_0 \sqrt{\epsilon_r}} - 2\Delta l.$$

the dielectric constant of substrate, f_0 is the target center frequency, and ϵ_e is the effective dielectric constant. Consider

The geometry of the proposed antenna is as shown in Figure 1. The antenna consists of rectangular conducting slots on patch and two on the ground. The design procedure begins with the radiating patch with substrate, ground plane, and a feed line. It has been printed on a FR4 substrate with 1.6 mm thickness that contains relative permittivity 4.60, relative permeability 1, and dielectric loss tangent 0.02. A rectangular slot is cut from one side of the copper patch to another. Another two rectangular slots are also cut from the middle of the patch. Five lateral rectangular slots are also cut from the ground plane.



Figure 1: The proposed antenna (a) top view and (b) Bottom view.

Thus, the proposed double inverted F-shape microstrip patch antenna is achieved. Two resonant frequencies, 11.32 GHz and 14.96 GHz, are obtained adjusting length, width, and slots of the proposed antenna endlessly. Here, microstrip line is used to provide feeding to the proposed antenna.

The subminiature version A (SMA) connector that contains 50 Ω is conducted at the end of antenna feeding line for input RF signal. The input impedance of the proposed antenna is as shown in Figure 2. Finally the optimal dimensions have been determined as follows: $L = 40$ mm, $W = 40$ mm, $R = 6$ mm, $S_1 = 10$ mm, $S_2 = 16.5$ mm, $S_3 = 12$ mm, $W_1 = 4$ mm, $W_2 = 7$ mm, $L_g = 40$ mm, $W_g = 40$, $W_3 = 18$ mm, $W_4 = 6$ mm, $W_5 = 8$ mm, $W_6 = 4$ mm, and $W_7 = 7$ mm. The proposed prototype of the antenna is shown in Figure 3.



Figure 2: Input impedance of the proposed antenna.

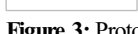


Figure 3: Prototype of the proposed antenna.

The return loss of simulation with different substrate materials is demonstrated in Figure 4. Teflon is a fluorine plastic that is very slippery with physical properties. It is a

brand for polytetrafluoroethylene (PTFE). When we used Teflon (tm) as a substrate material, there was no resonance on the lower band. But, resonance was found at 14.68 GHz center frequency on the upper band where -10 dB bandwidth is 1.36 GHz.



Figure 4: Comparisons of simulated return loss with different materials.

Duroid (tm) is a circuit material with high frequency that is filled with PTFE composite. There are many benefits of Duroid (tm) substrate material such as low outgassing for space applications, low moisture absorption, and low electrical loss. This material is extensively used in space satellite transceivers, radar systems based on ground and airborne, missile guidance systems, and military radar systems. When we used Duroid (tm) as a substrate material, there was no resonance on the upper band. But, resonance was found at 12.40 GHz center frequency on the lower band where -10 dB bandwidth is 1.36 GHz.

Bakelite is one type of plastic that is a thermosetting phenol formaldehyde resin. It is made from synthetic components achieved from an elimination reaction of phenol with formaldehyde. It has several uses such as in radio, electrical insulators, and telephone casings. When we used Bakelite as a substrate material, there was no resonance on the lower band. But, resonance was found at 14.40 GHz center frequency on the upper band where -10 dB bandwidth is 1.68 GHz (14.64 GHz–13.96 GHz).

Aluminum is a silvery soft, white ductile material. Aluminium is extensively used in transportation, aerospace industry, and structural materials. It has low density and ability to resist corrosion for which it is popular. When we used aluminum as a substrate material, there was no resonance on the lower band. But, resonance was found at 14.32 GHz centre frequency on the upper band where -10 dB bandwidth is 1.44 GHz (15.04 GHz–13.60 GHz).

Finally, FR4 has been used in the proposed design as substrate material. One resonance was achieved at 11.32 GHz center frequency on the lower band and another resonance at 14.96 GHz on the upper band. The dielectric properties of the materials have been listed in Table 1.



Table 1: Dielectric properties of substrate materials.

A parametric study has been done to observe the effects of the proposed antenna parameters. Mainly, the effects of the different parameters on the return loss have been observed.

Figure 5 shows the reflection coefficient for different values of R . It includes $L = 40$ mm, $W = 40$ mm, $S_1 = 10$ mm, $S_2 = 16.5$ mm, $S_3 = 12$ mm, $W_1 = 4$ mm, $W_2 = 7$ mm, $L_g = 40$ mm, $W_g = 40$, $W_3 = 18$ mm, $W_4 = 6$ mm, $W_5 = 8$ mm, $W_6 = 4$ mm, and $W_7 = 7$ mm with R . It was shown that resonances were shifted on both of the lower and upper bands using the value of radius as 5 mm and 7 mm.



Figure 5: Reflection coefficient with different values of radius, R .

By using $R = 6$ mm, desired dual band has been obtained with improved bandwidth on both of the lower and upper bands. That is why the optimized value of radius R is 6 mm.

The reflection coefficient for different values of W_5 is as shown in Figure 6. It includes $L = 40$ mm, $W = 40$ mm, $R = 6$ mm, $S_1 = 10$ mm, $S_2 = 16.5$ mm, $S_3 = 12$ mm, $W_1 = 4$ mm, $W_2 = 7$ mm, $L_g = 40$ mm, $W_g = 40$, $W_3 = 18$ mm, $W_4 = 6$ mm, $W_6 = 4$ mm, and $W_7 = 7$ mm with W_5 . It was seen from the graph clearly that better coupling has been acquired at the upper band using the value of W_5 as 8 mm. That is why the optimized value is 8 mm.



Figure 6: Reflection coefficient with different values of W_5 .

Figure 7 shows the reflection coefficient for different values of W_7 . It includes $L = 40$ mm, $W = 40$ mm, $R = 6$ mm, $S_1 = 10$ mm, $S_2 = 16.5$ mm, $S_3 = 12$ mm, $W_1 = 4$ mm, $W_2 = 7$ mm, $L_g = 40$ mm, $W_g = 40$, $W_3 = 18$ mm, $W_4 = 6$ mm, $W_5 = 8$ mm, and $W_6 = 4$ mm with W_7 . It was observed that the width of the microstrip line has greater significance to the coupling at the entire frequency bands. The coupling can be achieved when W_7 is 7 mm.



Figure 7: Reflection coefficient with different values of W_7 .

3. Results and Discussion

The anechoic chamber used in this study which was conducted by the microwave laboratory, at the Institute of Space Science (ANGKASA), UKM, Malaysia, had been illustrated in Figure 8. The dimensions of this anechoic chamber are $5.5 \times 4.5 \times 3.5$ m³. A reference antenna, a horn antenna, was used in this analysis that was double ridge guided. Pyramidal shaped absorbers have been used on the walls, ceiling, and floor with less than -60 dB reflectivity. The diameter of the turntable is 1.2 m. A vector network analyzer (VNA) (model number: Agilent E8362C) has been used for the measurements with a range of up to 20 GHz. In this way, the prototype of the Ω shaped proposed antenna has been measured in a standard far-field testing environment.



Figure 8: The photograph of anechoic chamber for prototype measurement.

The return loss with measurement and simulation of the proposed microstrip antenna has been demonstrated in Figure 9. The -10 dB bandwidths of 2.12 GHz from 10.92 GHz to 13.04 GHz and 1.08 GHz from 14.40 GHz to 15.48 GHz have been achieved from the measurements which show that at the lower band the resonance shifted from 11.32 GHz to 11.44 GHz and the bandwidth slightly decreased. Moreover, at the upper band the resonant frequency shifted from 14.96 GHz to 14.84 GHz and the bandwidth decreased from 1.16 GHz to 1.08 GHz, while the return loss value decreased at resonance frequency.

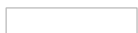


Figure 9: Comparisons between simulated and measured return loss on FR4 material.

Gain of the proposed antenna has been shown in Figure 10. Figure 10 has illustrated that 7.82 dBi achieved at the first resonance for 11.44 GHz and 5.66 dBi at the second resonance 14.84 GHz. In addition, the gain for the upper band is less than that for the lower band. Figure 11 shows VSWR of the proposed antenna. The value of VSWR is less than 2 that is found from the graph apparently. It is a desired value. Figure 12 has shown the radiation efficiency of the proposed antenna. In Figure 11, the average lower band efficiency is 79.76% whereas 80.36% is the higher band efficiency. It can also be observed that lower band radiation efficiency is smaller than

the higher band one.



Figure 10: Gain of the proposed antenna.



Figure 11: VSWR of the proposed antenna.



Figure 12: Radiation efficiency of the proposed antenna.

Figure 13 has been shown the current distribution of the proposed antenna for (a) 11.32 GHz and (b) 14.96 GHz. It can be seen that a large amount of current flows at feeding line. Electric field has been created much in this point. Current distribution is more stable in lower band than in upper band. The creation of electric field near slots is reasonable. As a result, excitation is strong in the entire parts of the antenna on both the lower band and the upper band.



Figure 13: Current distribution at (a) 11.32 GHz and (b) 14.96 GHz.

The radiation pattern of the proposed antenna with measurement has been demonstrated in Figure 14 for (a) 11.32 GHz at E-plane, (b) 11.32 GHz at H-plane, (c) 14.96 GHz at E-plane, and (d) 14.96 GHz at H-plane. The E_ϕ and E_θ fields indicate the cross-polar and copolar components, respectively. The effect of cross-polarization in radiation pattern is lower microstrip antenna. The cross-polarization effect is higher in the H-plane for both resonances. When frequency increases, the effect increases interpreting from the radiation pattern simply. Moreover, almost omnidirectional and symmetrical radiation patterns have been attained along both E-plane and H-plane.



Figure 14: Radiation patterns of the proposed antenna, (a) 11.32 GHz at E-plane, (b) 11.32 GHz at H-plane, (c) 14.96 GHz at E-plane, and (d) 14.96 GHz at H-plane.

It has been observed that the same radiation pattern exists over the X- and Ku-bands. The obtained radiation patterns denote that the proposed antenna delivers linear polarization where the level of cross-polarization is lower than that of copolarization in all of the simulated radiation patterns. When the radiation pattern of a microstrip antenna is symmetric and omnidirectional, it faces some reasonable benefits. One is that resonance would never be shifted at different directions and a large amount of stable power would be at the direction of broadside beam. Another advantage is that the radiation pattern would be more durable on the operational bands.

The phase variation of the proposed antenna is plotted in Figure 15. It is realized from the graph that the proposed antenna has the phase variation that is linear across both the upper and the lower operating frequency bands. This phase variation indicates that all the frequency components of the signal have the same pulse distortion due to the same propagation delay. Comparisons between existing and proposed antennas have been tabulated in Table 2.



Table 2: Comparisons between existing and proposed antennas.



Figure 15: Phase value of the proposed antenna.

The Smith chart of the proposed antenna is shown in Figure 16. Two resonances m_1 and m_2 are identified clearly from this chart which has validated the evidences.



Figure 16: Smith chart of the proposed antenna.

4. Conclusion

A 40 mm × 40 mm double inverted F-shape patch antenna has been discussed in this paper for dual band-operation. The measured impedance bandwidths (2 : 1 VSWR) 2.12 GHz on the upper band and 1.08 GHz on the lower band with average gains of 7.82 dBi and 5.66 dBi have been achieved belonging to radiation efficiency 79.76% and 80.36%. Since the antenna layout is simple and straightforward, fabrication and measurement are comparatively easier. The generalized design procedure for the proposed antenna for dual frequency operation has also been improved than conventional. It is realized that a good combination has been focused between measurements and simulations that validate our proposed double F-shaped design concept. The patch resonator, compact size, stable radiation patterns, low cross polarization, efficiency with improved bandwidth, and higher gain have made the proposed double F-shaped antenna compatible for X-band and Ku-band applications.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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